

The German CFD Network on Nuclear Reactor Safety Research:

"Development and Application of CFD Modelling to Phenomena in the Primary Circuit of Pressurized Water Reactors"

Results & Perspectives

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Inhalt



- Motivation and Objectives
- Structure of the German CFD Network
- Partner & Organizations
- Results:
 - Model development
 - Validation
 - Experiments
- Communication
- Perspectives
- Summary and Future Directives

Motivation

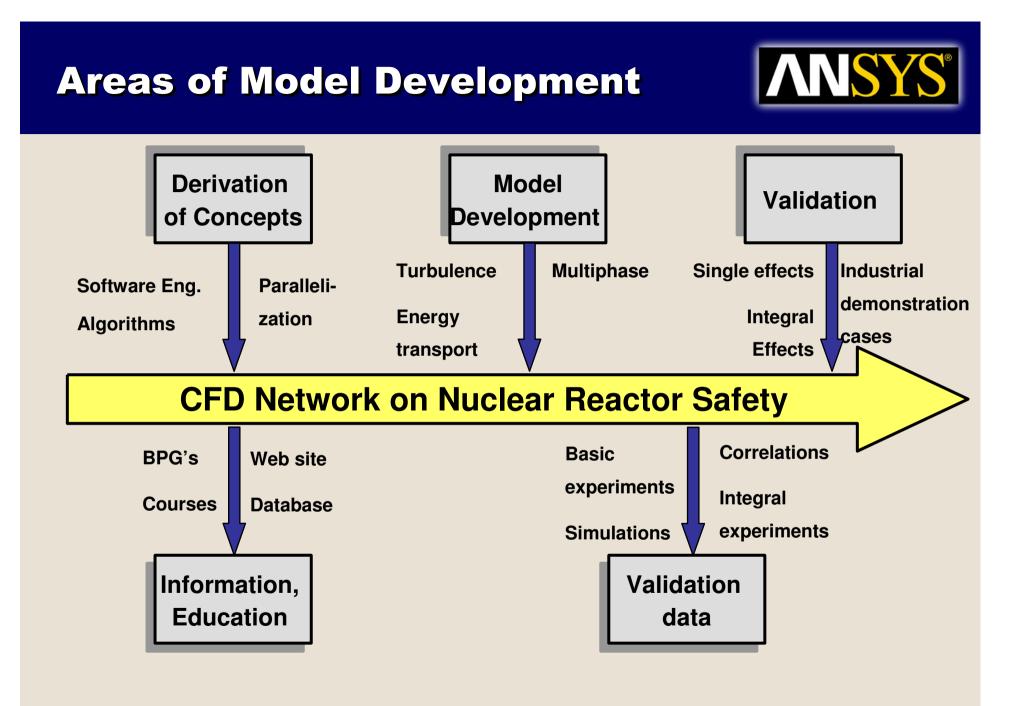


- Requirements:
 - Quantification of safety margins
 - Evaluation of measures for increase of power output
- Further development of simulation techniques
 - Multidimensional phenomena & applications
 - Two-phase flows
 - Phase interaction (mass, momentum, energy)
 - Validation
 - Code coupling
 - → Lumped parameter codes/1d codes (e.g. ATHLET, RELAP) & CFD codes
 - → Neutron kinetic codes & CFD codes
- Maximize the Efficiency of model development
 - Organize a collaborative project group of research institutions and software developers

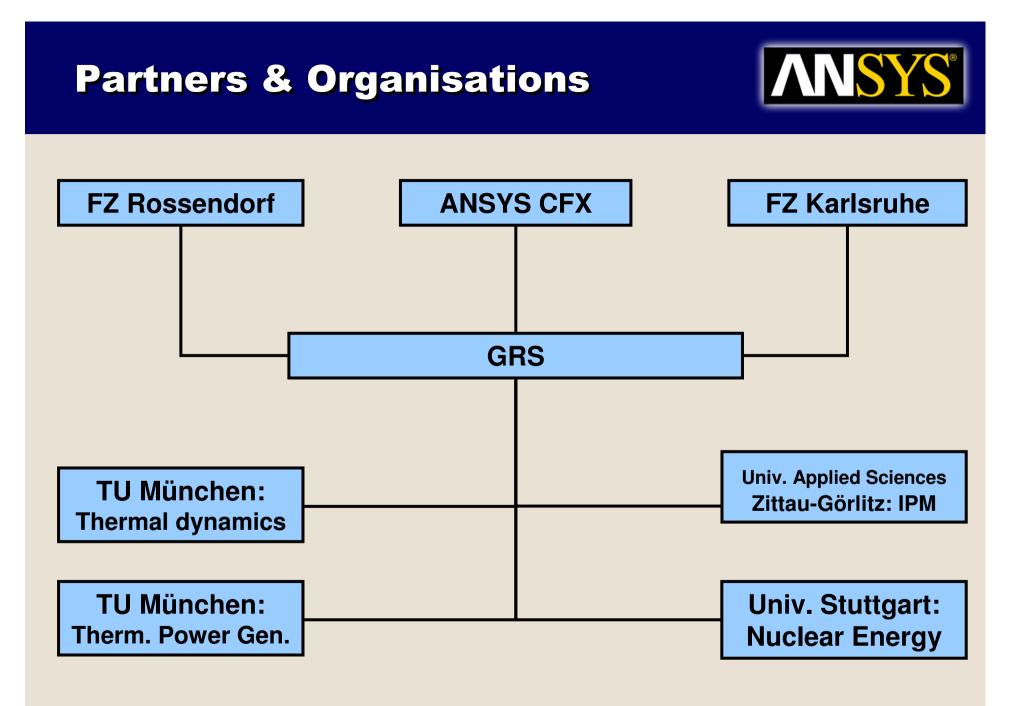
Objectives



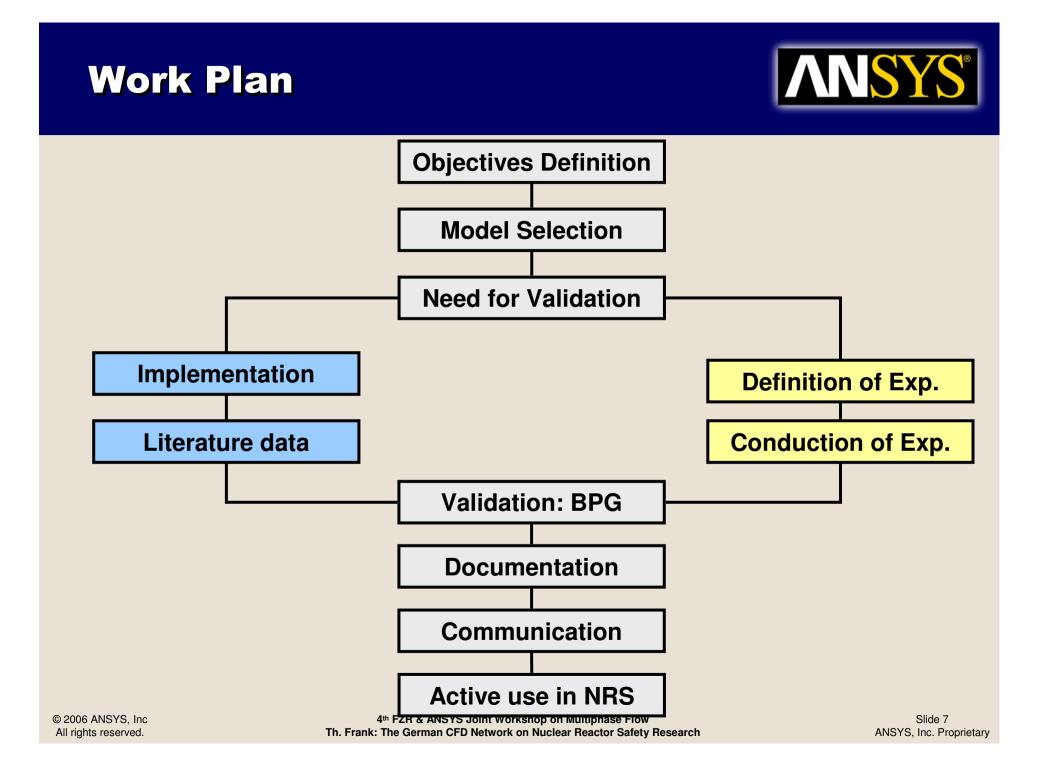
- Investigation of 3-dimensional flows in the primary circuit and in the containment of pressurized water reactors in a coordinated action
- Development & validation of two-phase flow models
- Coordination of new CFD related validation experiments
- Validation, provision & maintenance of a CFD code
- Development of Best Practice Guidelines (BPG) and check lists for model application
- Coupling of the CFD code with ATHLET



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Objectives Definition – Validation Test Cases



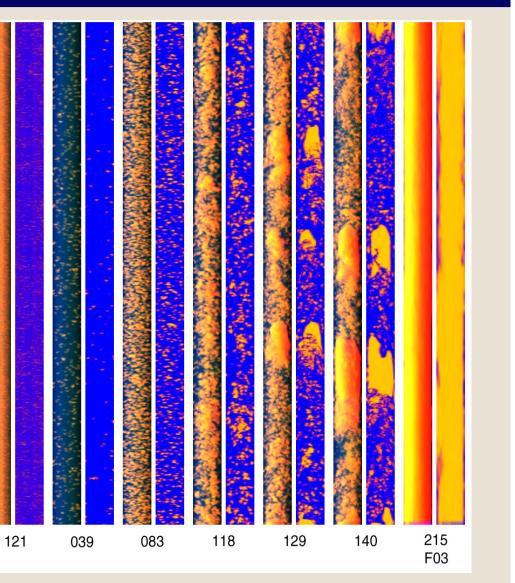
- Two-phase flows with lower void fraction
 - Vertically upward
 - Vertically downward
 - Horizontal, con-current
 - Horizontal counter-current
- Two-phase flows with higher void fraction
 - Vertically upward
 - Vertically downward
 - Horizontal, con-current
 - Horizontal counter-current

- Free Surface Flows
 - Horizontal con-current
 - Horizontal counter-current
 - Impinging Jets (Downcomer)
 - Free Jets (ECC)
- Flows with phase change
 - Condensation
 - Evaporation
 - Flashing
 - Boiling

Vertical Pipe Flows



- Experiments
 - FZR
 - MTLoop & TOPFLOW Facility
- Modeling & Validation
 - FZR
 - ANSYS CFX
- Target variables
 - Volume fraction
 - Gas velocity
 - Water velocity
 - Bubble size distributions



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Investigation on MT-Loop & TOPFLOW Test Matrices



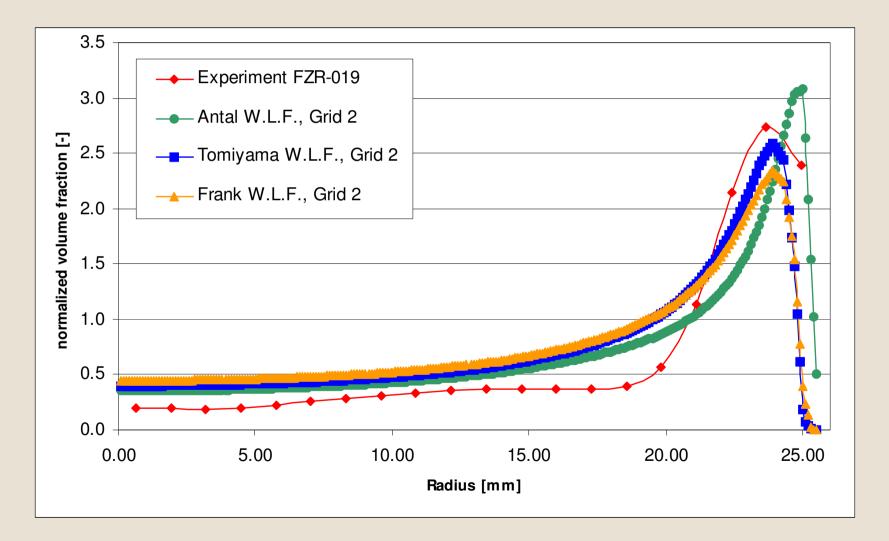
Testcases predicted with CFX-5.7.1/CFX-10.0:

Leerrohrgeschwindigkeit Gas J_G in m/s

| m/s | | 0,0025 | 0,0040 | 0,0062 | 0,0096 | 0,0151 | 0,0235 | 0,0368 | 0,0574 | 0,0898 | 0,140 | 0,219 | 0,342 | 0,534 | 0,835 | 1,305 | 2,038 | 3,185 | 4,975 | 7,772 | 12,14 |
|------------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| in π | 4,047 | 011 | 022 | 033 | 044 | 055 | 066 | 077 | 088 | 099 | 110 | 121 | 132 | 143 | 154 | 165 | 176 | 187 | 198 | 209 | 220 |
| Jw İ | 2,554 | 010 | 021 | 032 | ø43 | 054 | 065 | 076 | 087 | 098 | 109 | 120 | 131 | 142 | 153 | 164 | 175 | 186 | 197 | 208 | 219 |
| ser | 1,611 | 009 | 020 | 031 | 042 | 053 | 064 | 075 | 086 | 097 | 108 | 119 | 130 | 141 | 152 | 163 | 174 | 185 | 196 | 207 | 218 |
| Was | 1,017 | 008 | 019 | 030 | 041 | 052 | 063 | 074 | 085 | 096 | 107 | 118 | 129 | 140 | 151 | 162 | 173 | 184 | 195 | 206 | 217 |
| - · · · | 0,641 | 007 | 018 | 029 | 040 | 051 | 062 | 073 | 084 | 095 | 106 | 117 | 128 | 139 | 150 | 161 | 172 | 183 | 194 | 205 | 216 |
| digk | 0,405 | 006 | 017 | 028 | 039 | 050 | 061 | 072 | 083 | 094 | 105 | 116 | 127 | 138 | 149 | 160 | 171 | 182 | 193 | 204 | 215 |
| windigkeit | 0,255 | 005 | 016 | 027 | 038 | 049 | 060 | 071 | 082 | 093 | 104 | 115 | 126 | 137 | 148 | 159 | 170 | 181 | 192 | 203 | 214 |
| esch | 0,161 | 004 | 015 | 026 | 037 | 048 | 059 | 070 | 081 | 092 | 103 | 114 | 125 | 136 | 147 | 158 | 169 | 180 | 191 | 202 | 213 |
| ırge | 0,102 | 003 | 014 | 025 | 036 | 047 | 058 | 069 | 080 | 091 | 102 | 113 | 124 | 135 | 146 | 157 | 168 | 179 | 190 | 201 | 212 |
| errohrg | 0,0641 | 002 | 013 | 024 | 035 | 046 | 057 | 068 | 079 | 090 | 101 | 112 | 123 | 134 | 145 | 156 | 167 | 178 | 189 | 200 | 211 |
| Lee | 0,0405 | 001 | 012 | 023 | 034 | 045 | 056 | 067 | 078 | 089 | 100 | 111 | 122 | 133 | 144 | 155 | 166 | 177 | 188 | 199 | 210 |

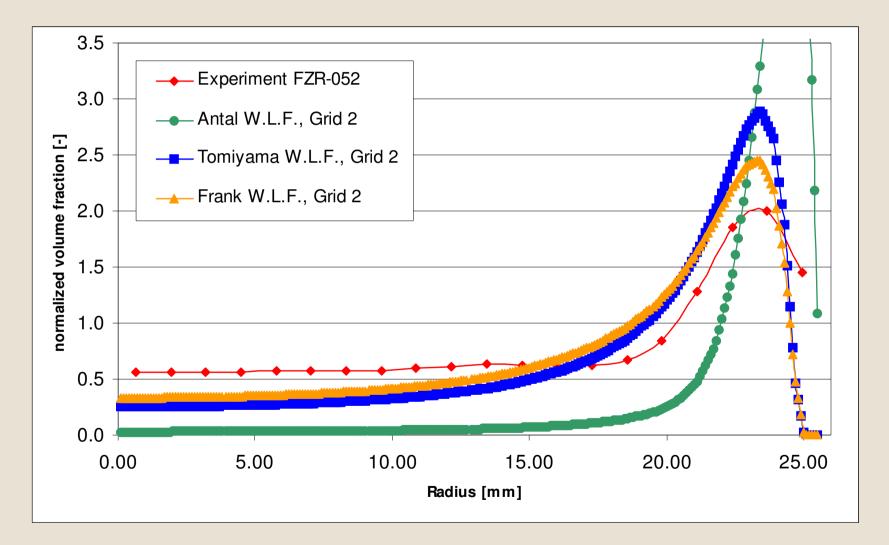










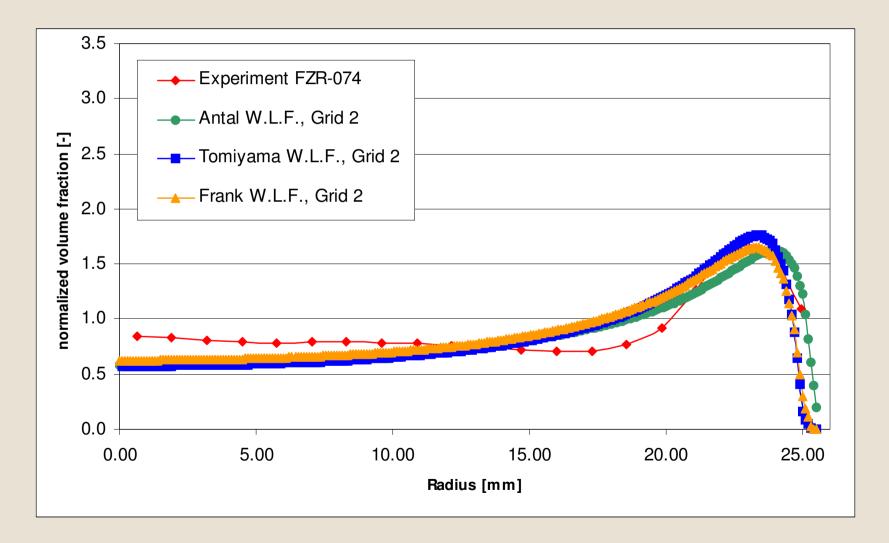


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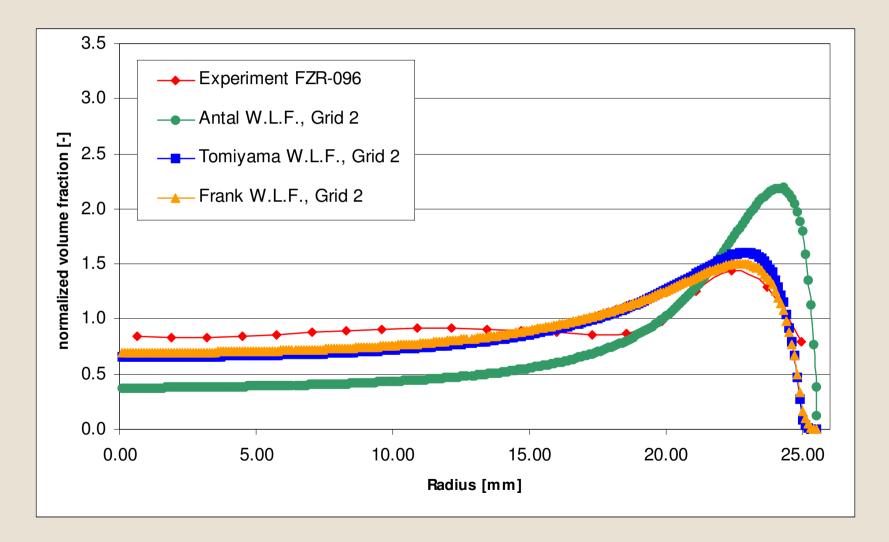


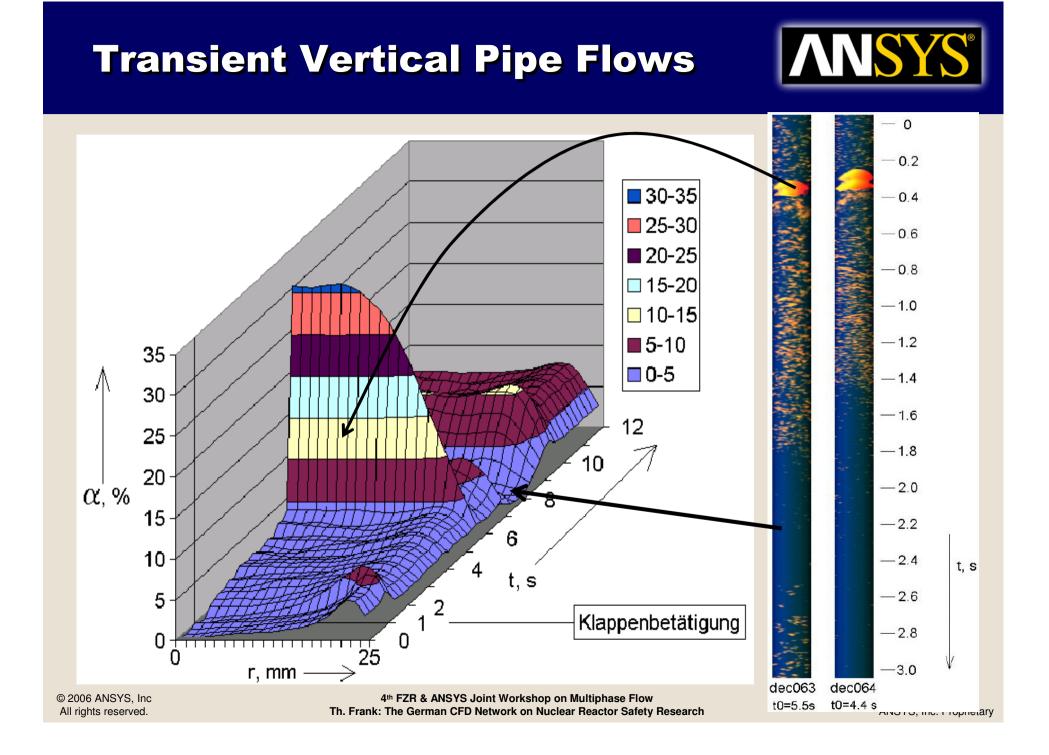


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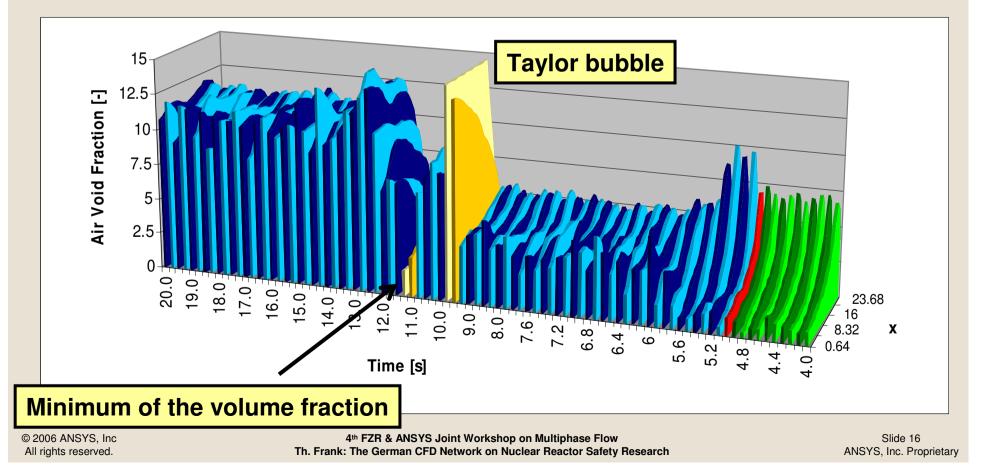




Transient Vertical Pipe Flows



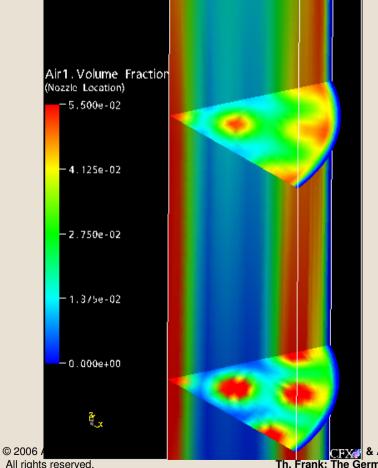
- Reduction in water mass flow rate at T = 5 s
- Transient radial volume fraction distribution of bubbly phase

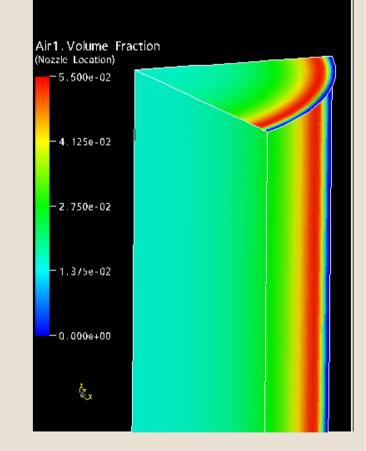


Transient Vertical Pipe Flows



- Gas superficial velocity 1.02 m/s
- Inlet boundary conditions





Measurement cross section @ t = 4.5 s

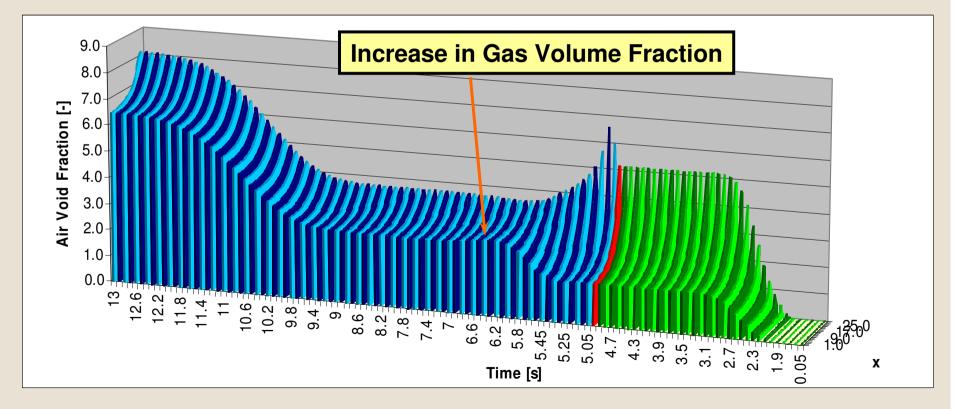
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Transient Vertical Pipe Flows

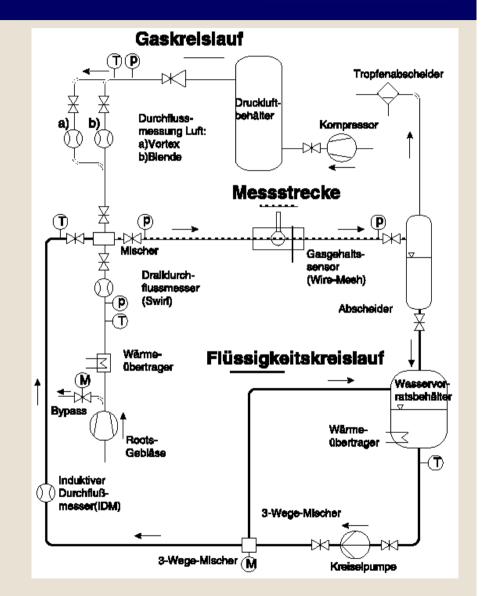


- CFD Prediction
- Qualitative agreement in system
 behavior
- Transition between volume fraction profiles
- Taylor bubble not observed in CFD (pressure-sparger interaction?)



Horizontal Pipe & Channel Flows **MSYS**

- Experiments
 - TU München (Thermal dynamics)
 - FZR
- Modeling & Validation
 - TU München (Thermal dynamics)
 - FZR
 - CFX
- Target Variables
 - Volume fraction
 - Gas velocities
 - Water velocities

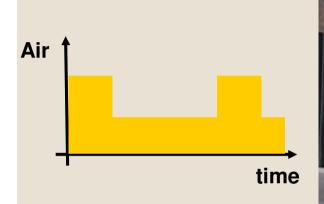


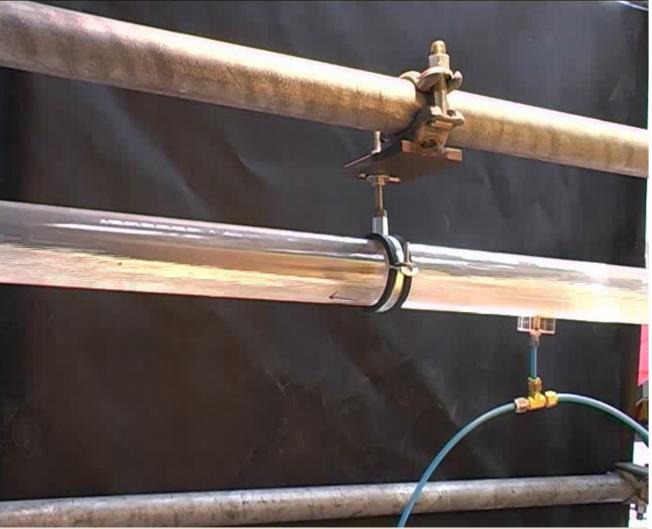
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Experimental Test Facilities @ TU Munich



Regular slug flow with defined inlet BC's





Edurne Carpintiero, TD, TUM © 2006 ANSYS, Inc All rights reserved.

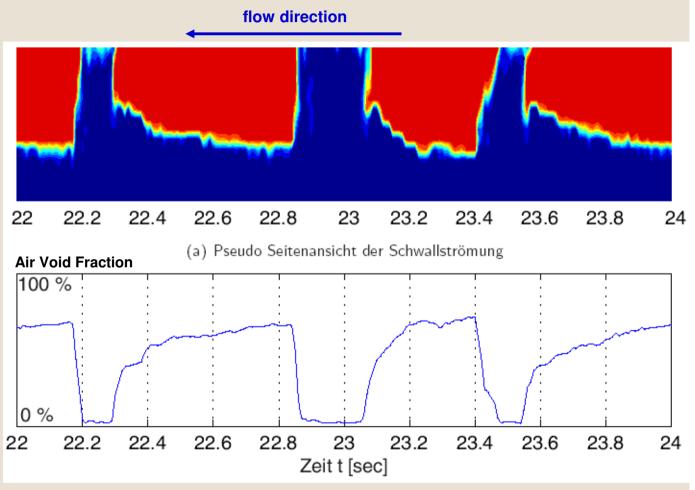
By courtesy of

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Transient Slug Flow: Test case conditions



- $\dot{M}_L = 2.363 \ kg \ / \ s$
- $\dot{M}_{G} = 2.9 \ g \ / \ s$
- j_G=j_L=1 m/s
- air void fraction r_G=0.5
- air/water inlet pressure: p=1.055 bar
- slug front velocity: 2.7 m/s
- mean slug length:
 1.8m
 (gas: 1.45m
 water: 0.35m)
- slug frequency: 1.5 Hz
- pressure loss: ~700 Pa/m

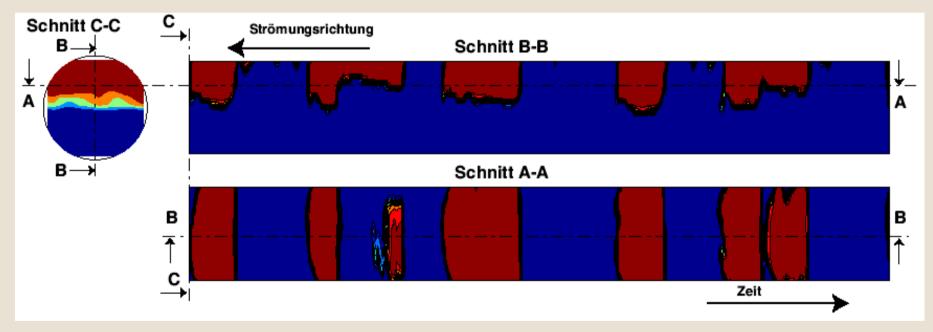


By courtesy of Thomas Lex, TD, TUM

Transient Air Volume Fraction Measurements with Wire Mesh Sensors



 this measurements correspond to j_G=j_L=1 m/s and an air and water volume fraction of 0.5



Experiments by Thomas Lex, TD, TUM

Slug Flow Simulations

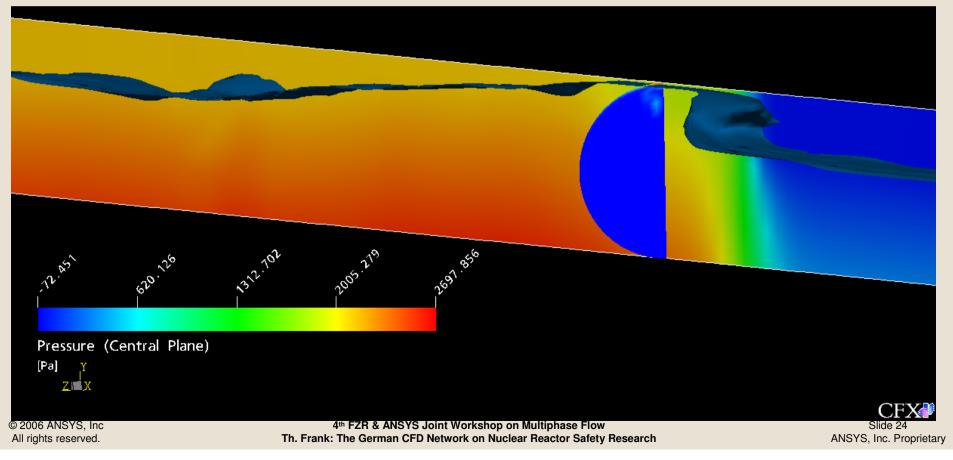


| No. | Pipe | Spatial mes | h resolution | No. of | Test case conditions | | | | |
|--------|-----------------|---|-------------------------------------|------------|--|--|--|--|--|
| length | | Grid cells in pipe cross- section | Grid cells in axial direction | grid cells | | | | | |
| 1 | 1.0m / 4.0 m | 249 | 250 | 73.500 | Periodic BC's; Sinusoidal agitated free surface (initialization); Prescribed pressure loss of 800 Pa/m | | | | |
| 2 | 8.0m | 249 | 500 | 147.000 | Massflow BC's; Sinusoidal agitated free surface at inlet | | | | |
| 3 | 8.0m | 249 | 500 | 147.000 | as 2), but without surface agitation | | | | |
| 4 | 8.0m | 249 | 500 | 147.000 | Massflow BC's; Phases homogeneously mixed at inlet; No agitation | | | | |
| 5 | 8.0m | 249 | 500 | 147.000 | Massflow BC's; Phases homogeneously mixed at inlet; Transient change in air void fraction between 0.5 and 0.7 | | | | |

Slug Flow Simulation -Mass Flow Boundary Condition



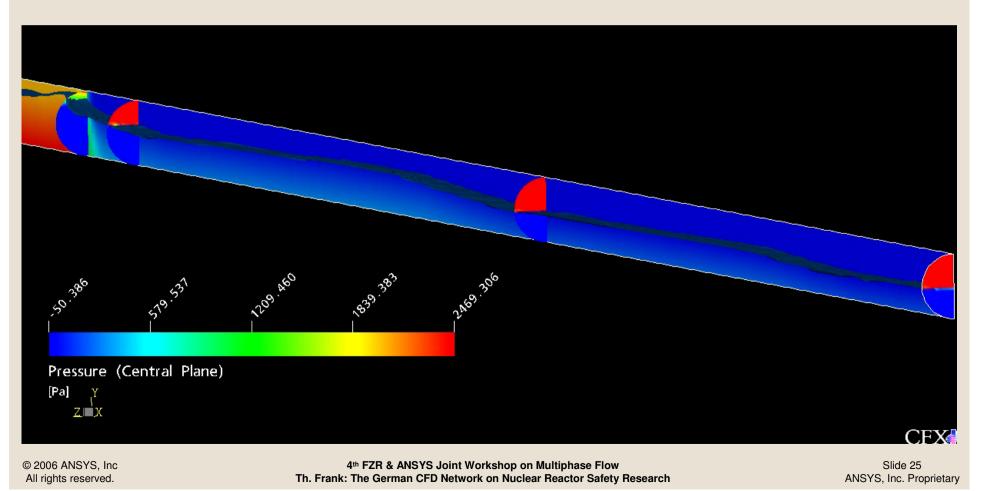
- Sinusoidal free surface perturbation (initialization and inlet BC's)
- Transient simulation of 7.0s real time
- Slug formation after ~4.0s at x~4.0m
- Stable slug propagation; slug front/tail are continuously changing



Slug Flow Simulation -Mass Flow BC's (cont.)



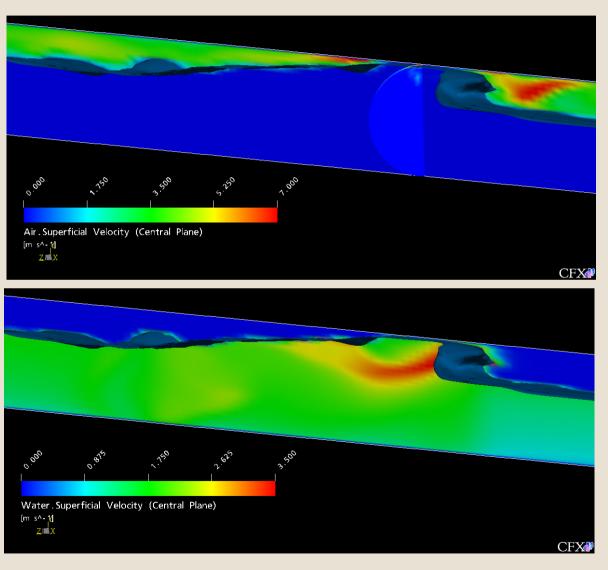
- Detail of slug flow formation and propagation (T = 3.4s,...,4.7s)
- Strong pressure gradients at slug front



Slug Flow Simulation -Mass Flow BC's (cont.)



 Superficial velocity distribution in and around a propagating slug



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Slug Flow Simulation -Mass Flow BC's (cont.)



First comparison with experimental data:

- Start of slug formation at ~4.0m from the inlet
- Difficult to reproduce experimental setup in CFD
 - Inlet BC's (e.g. phase mixing, inlet turbulence properties)
 - Pressure outlet conditions (pipes & tanks downstream of test section)
- Quantitative comparison difficult for strong transient flow
 - Small number of computed slugs
 - Slug length affected by limited pipe length and/or inlet conditions

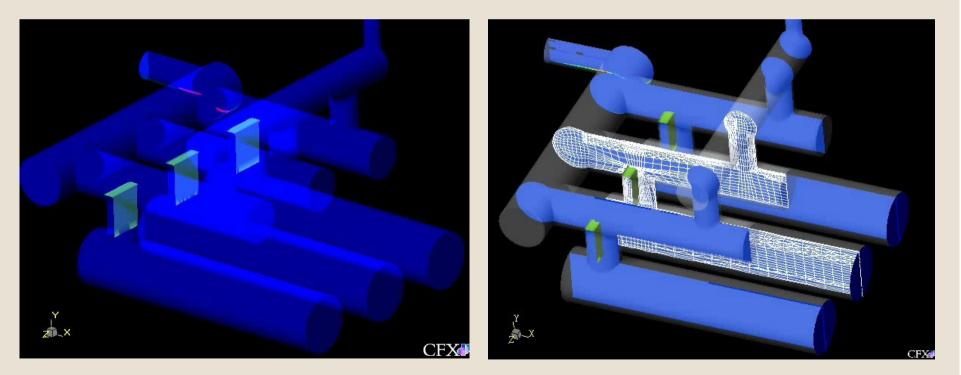
| | numerical simulation | experiment | | |
|--------------------------|--|------------|--|--|
| slug period | ~2.7m | ~1.8m | | |
| slug transition velocity | ~3.0 m/s | ~2.7 m/s | | |
| pressure loss | ~2000 - 2800 Pa on the last 4m, 2 slugs → ~500 - 700 Pa/m | ~700 Pa/m | | |
| | (strong transient) | | | |

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Application to Oil & Gas Technology: Slug Catcher Operation



- No liquid carry-over to gas outlet
 - first separation finger (nearest symmetry plane) partially fills with liquid
 - other fingers receive less liquid



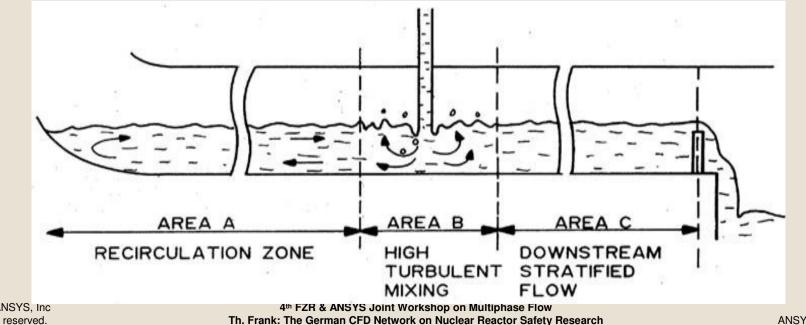
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Free Surface Flows



- ECC Injection: •
 - Impinging jets
 - Free jet
 - Stratified flow
 - Turbulent mixing

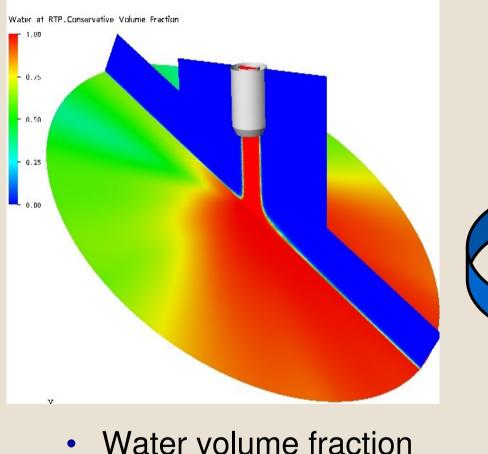
- Experiments: •
 - Kvicinsky & Avellan, EPFL
- Simulations: •
 - CFX-5
 - SST-Modell
 - Free surface model

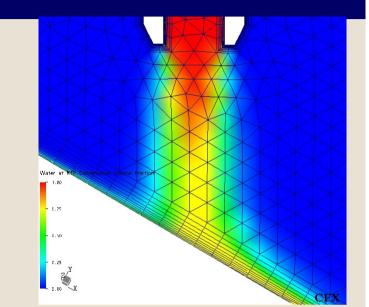


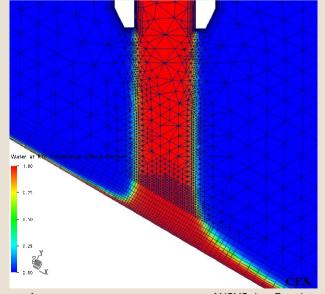
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Impinging Jet on Inclined Plate









- Water volume fraction
- Automatic grid refinement

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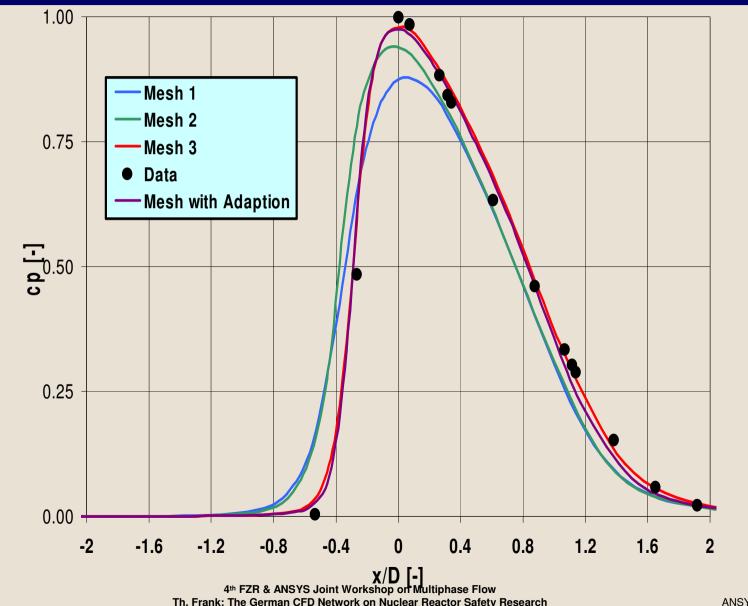
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Impinging Jet on Inclined Plate

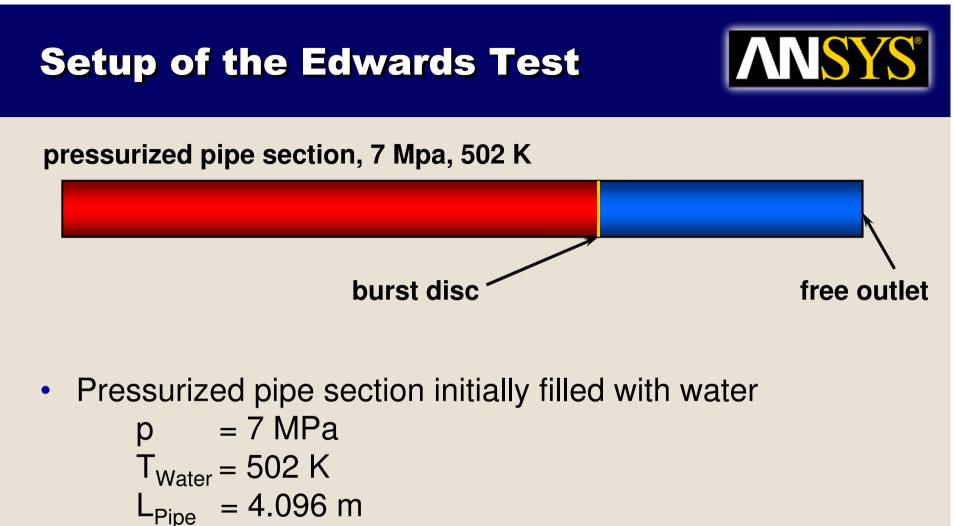
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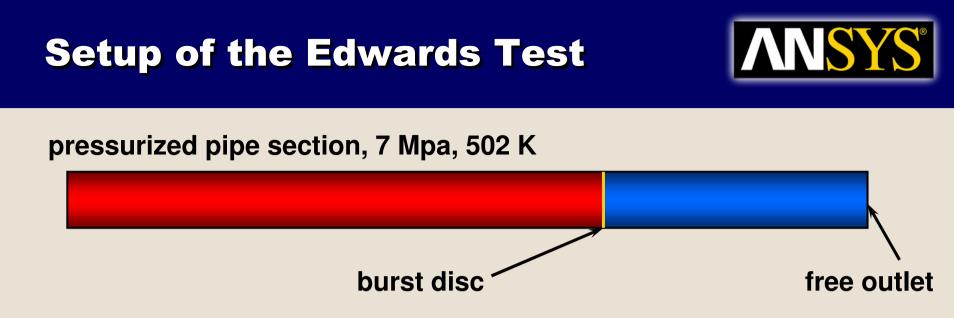




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- $D_{Pipe} = 0.0732 \text{ m}$
- Pressurized pipe closed with a burst disc (glass), broken at t=0.0s

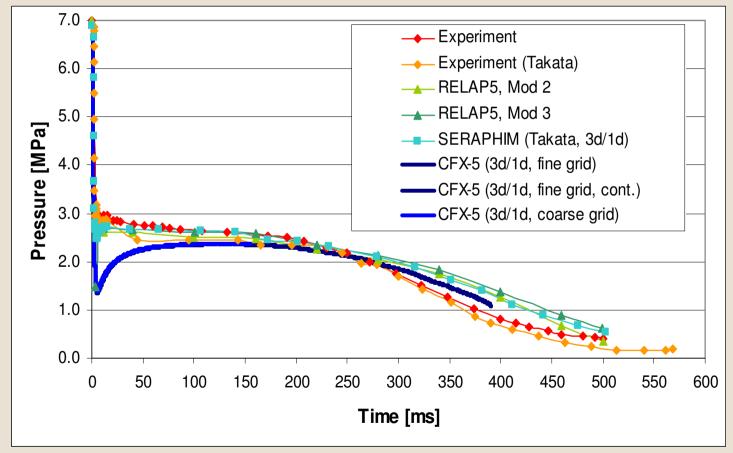


- Data of Edwards & Brien (1970), Takata & Yamaguchi (2003)
- Water-vapor flow
- Two-fluid model for bubbly flow
 - Thermal phase change model (bulk boiling) \rightarrow Flashing
 - Momentum transfer \rightarrow Grace drag
 - Heat transfer
- → Prediction of transient change of pressure, volume fraction, temperature

Pressure transient fine grid simulation; T=0.0s-0.392s



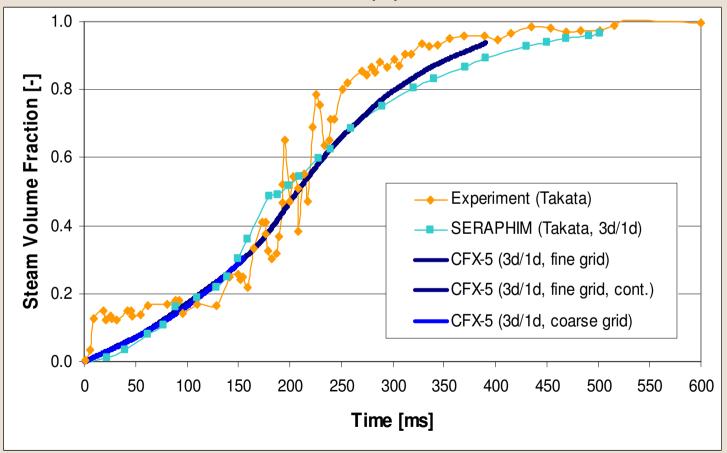
 comparison of pressure over time at the measurement location at x=1.469 m from the left pipe wall



Steam volume fraction transient fine grid simulation; T=0.0s-0.392s



 comparison of volume fraction over time at the measurement location at x=1.469 m from the left pipe wall



Further Projects



• GRS

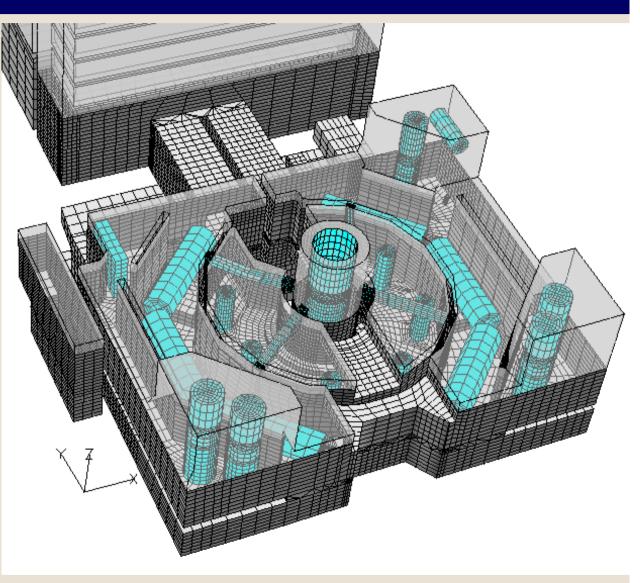
- Investigation on UPTF test cases (ECC)
- Containment flows,
 e.g. ISP 47 Step 2
- ANSYS & FZR
 - MUSIG-Models
 - Condensation models for free surface flows
 - Numerics improvements
 - Wall boiling by heat flux partitioning model

- University of Applied Sciences Zittau-Görlitz
 - Flow with insulation material; clogging and sedimentation
 - Experiments & simulations
- TU München, Thermal Power Technology
 - Condensation at free water jets
- University Stuttgart, Nuclear Power Engineering
 - Stratified counter-current flow (ECC in hot leg)

Containment Analysis VVER 440-213 (PAKS)



- LBLOCA with H₂ release
- 20 passive autocatalytic recombiners (PAR)
- bulk and wall condensation
- pressure peak suppression system
- 25 days on 8 processors (AMD)



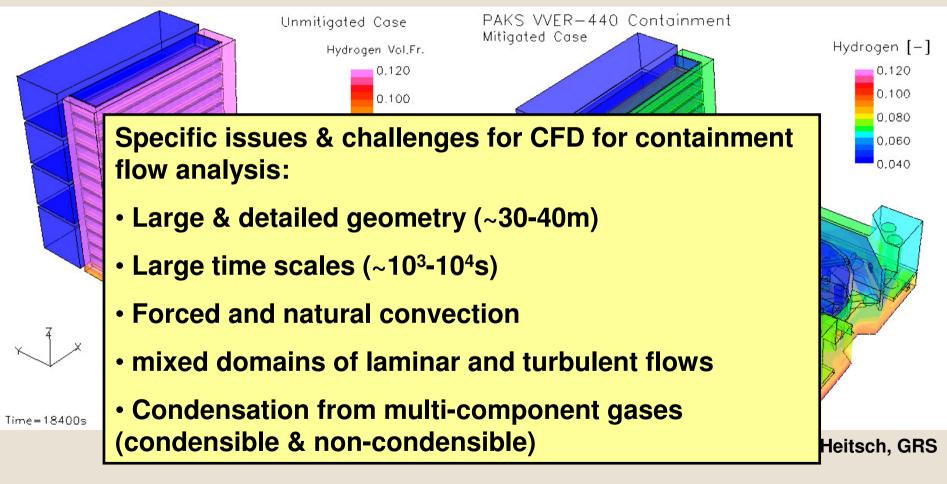
Courtesy of M. Heitsch, GRS

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Containment Analysis VVER 440-213 (PAKS)



Effect of H₂ passive autocatalytic recombiners:



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Communication



- http://domino.grs.de/cfd/cfd.nsf
- Contact: Martina Scheuerer, GRS
- Documents
 - Meeting protocols
 - Work plan definitions, collection of important publications
 - Validation test reports
- Measurement data
- Test case results
- CFD Network attracted further interest from
 - Nuclear Reactor Safety:
 → OECD, FISA, NURESIM, North-Net, CEA, EdF, Vattenfall, IRSN, NRG, TÜVs, Univ. Pisa
 - Process Technology:
 → Linde, BASF, Siemens

Perspective



- Project time frame 2006 2009
 - Funding of project partners: FZR, GRS, ANSYS
 - Cooperation with universities (driven by PhD program, 6 PhD's)
- Main topics of interest:
 - Flows with high volume fraction
 - Flows with phase change
 - Coupling of CFD with 1d/lumped parameter codes
 - Coupling of CFD with neutron kinetics code
 - Containment flows
- Networking with international partners:
 - NORTHNET Initiative
 - Cooperation with NRG, IRSN, PSI, ETHZ, ...
 - Approach funding for further initiatives from EC

Summary



- Motivation and major objectives
- Structure of the CFD Network on NRS

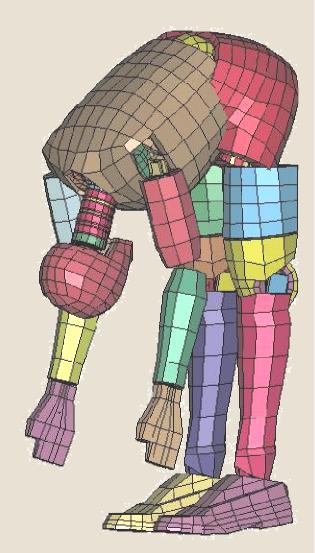


- Organisation \rightarrow Work plan defintion
- Results
 - Extensive validation of MPF models for vertical pipe flows
 - Horizontal pipe & channel flows
 - Free surface flows
- Active colaboration of all partners
- National and international interest





Thank You!



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